

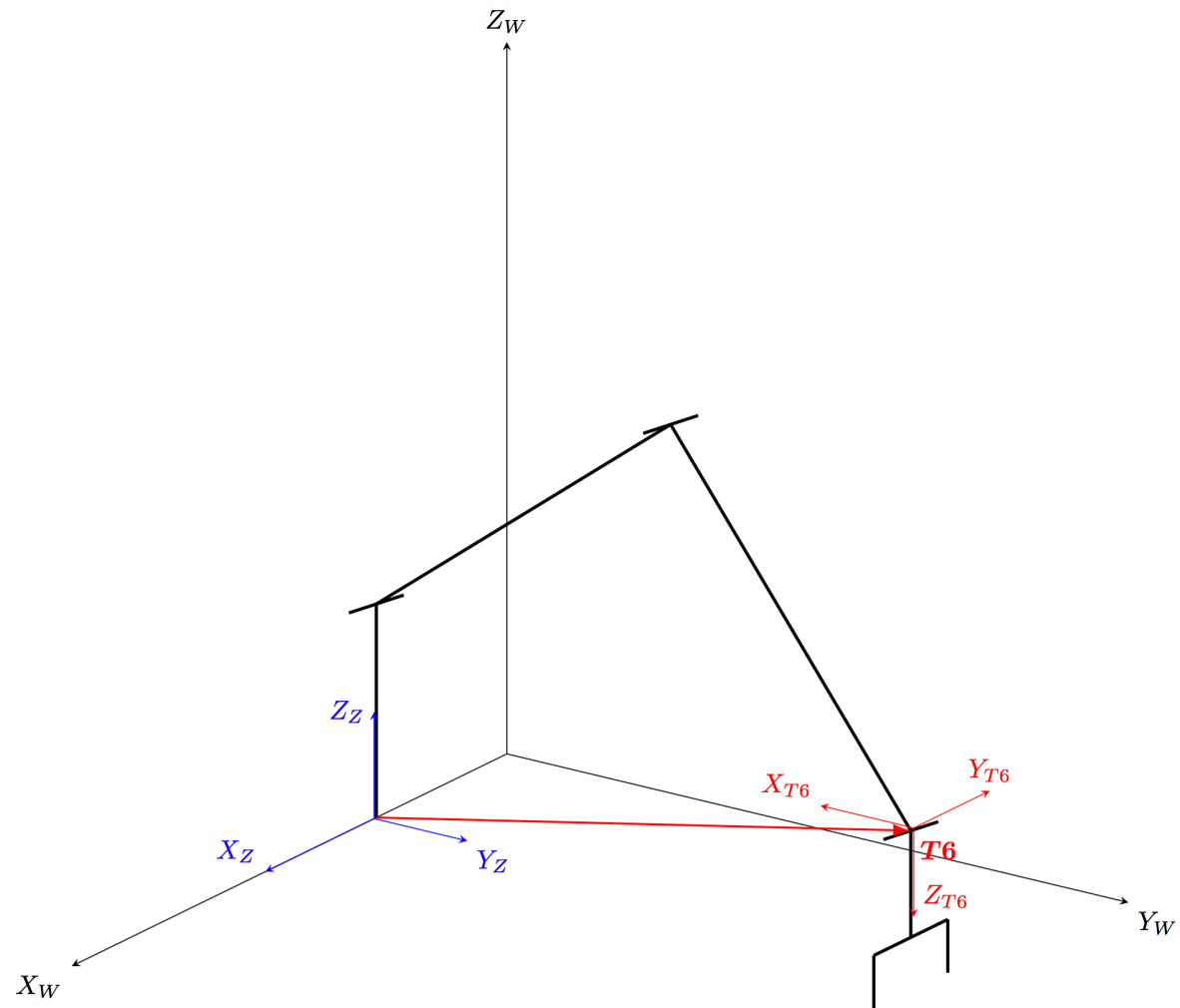
Introduction to Cognitive Robotics

Module 4: Robot Manipulators

Lecture 6: kinematics and inverse kinematics of the LynxMotion AL5D arm

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$T6$ The manipulator wrist

T_6 The position of the end of the manipulator
with respect to its base at Z

The **T_6** frame is a computable function of the joint variables

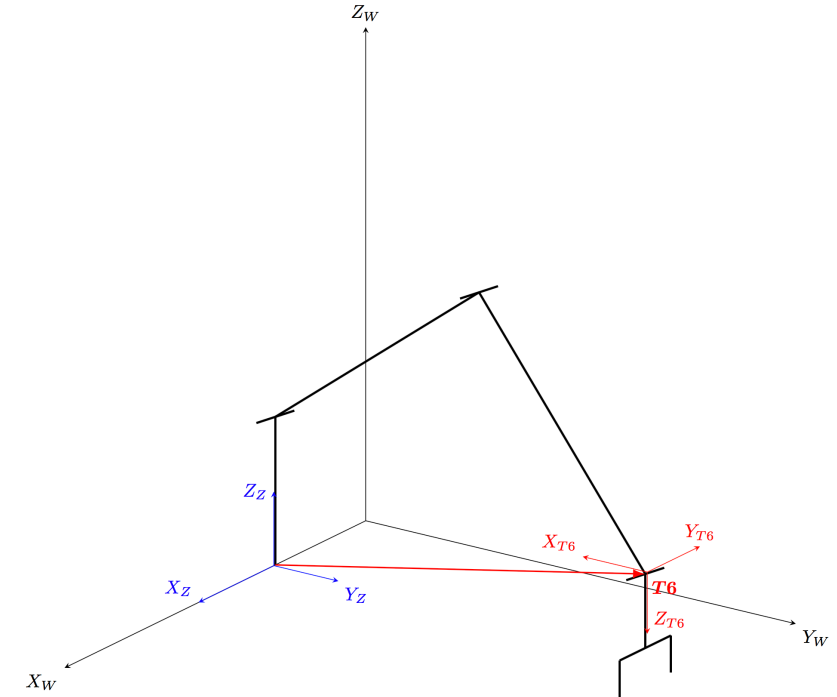
We need to define the relationship between Z and **T_6** in terms of the joint angles ...
i.e. we need to define the **manipulator kinematics**

Then we need to find the **inverse kinematic solution** the allows us to determine the joint values
that correspond to a given **T_6** :

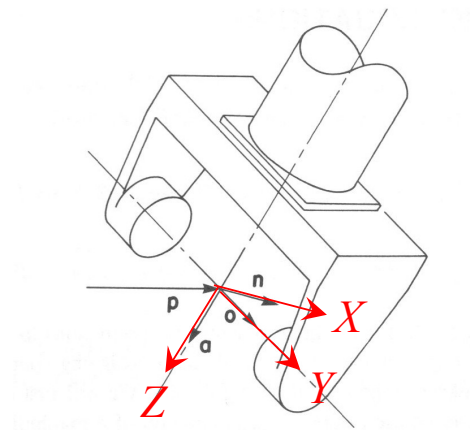
The joint variables are computed for a given **T_6** frame

Recall that there is a **convention** that the ***T6*** frame should be embedded in the manipulator

- with the **origin at the wrist**
- with the ***Z* axis directed outward from the wrist to the gripper**
- with the ***Y* axis directed in the plane of movement of the gripper** when it is opening and closing
- with the ***X* axis making up a right-hand system**



The same convention applies to the ***E*** frame that is embedded in a two-finger gripper (end-effector ... hence ***E***)



(Paul 1981)

Direction of *X* axis
 Direction of *Y* axis
 Direction of *Z* axis

$$E = \begin{bmatrix} n_x & o_x & a_x & p_x \\ n_y & o_y & a_y & p_y \\ n_z & o_z & a_z & p_z \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

n Normal
o Orientation
a Approach

Denavit-Hartenberg Representation

$$T_6 = {}^Z A_1 {}^{A_1} A_2 {}^{A_2} A_3 {}^{A_3} A_4 {}^{A_4} A_5 {}^{A_5} A_6$$

$$T_6 = A_1 A_2 A_3 A_4 A_5 A_6$$

${}^Z A_1$ position and orientation of link 1 w.r.t. the base

${}^{A_1} A_2$ position and orientation of link 2 w.r.t. A_1

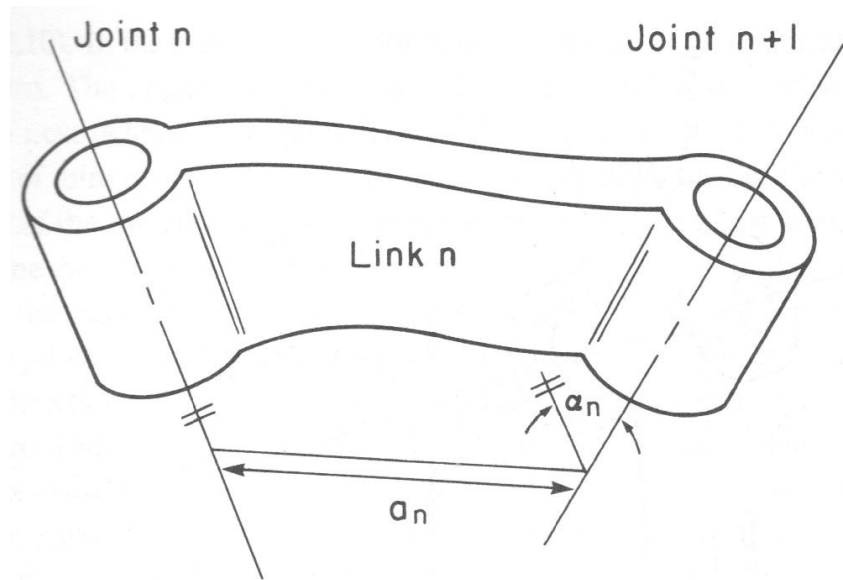
${}^{A_2} A_3$

${}^{A_3} A_4$

${}^{A_4} A_5$

${}^{A_5} A_6$ position and orientation of link 6 w.r.t. A_5

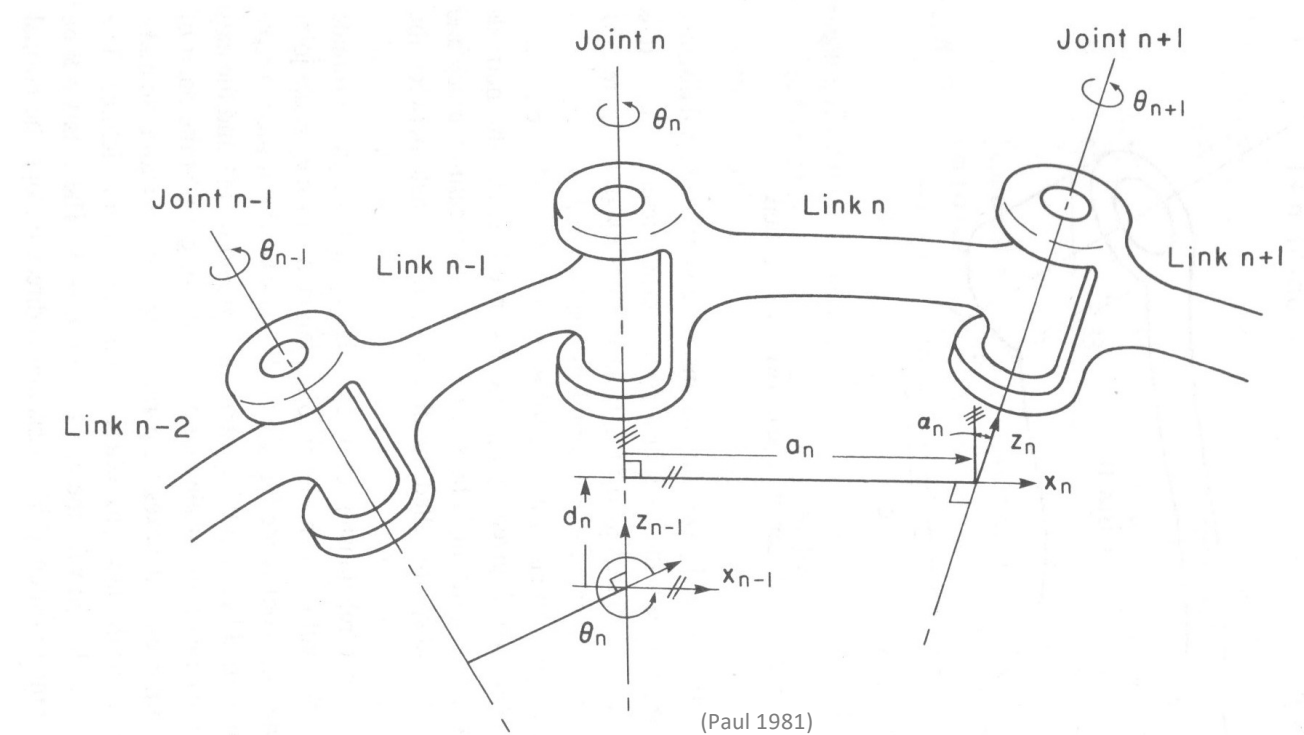
Denavit-Hartenberg Representation



(Paul 1981)

Link **length** (common normal distance) a_n

Link **twist** (angle between the two axes) α_n



A link axis has two normals to it, one for each link

d_n the distance between the normals along the joint n axis

θ_n the angle between the normals measured in a plane normal to the axis

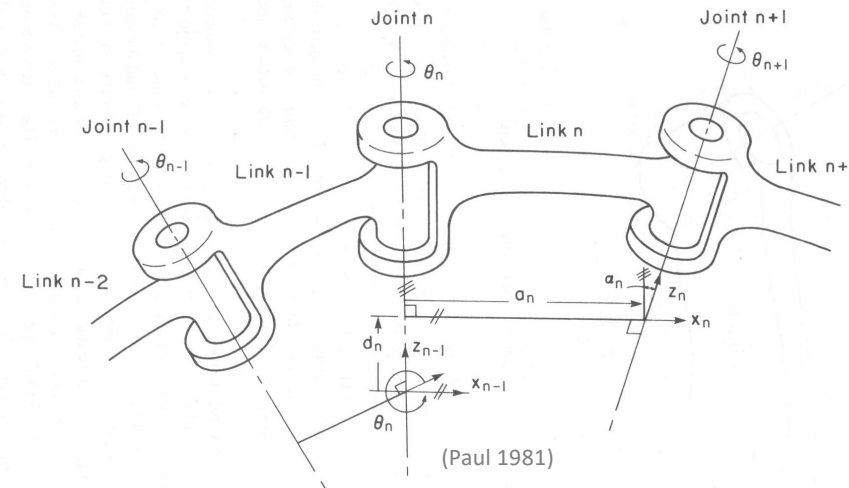
Denavit-Hartenberg Representation

- Assign coordinate frames to each link
- Determine the transformation from link $n-1$ to link n in terms of the four link parameters a_n α_n d_n θ_n

Denavit-Hartenberg Representation

Assign coordinate frames to each link

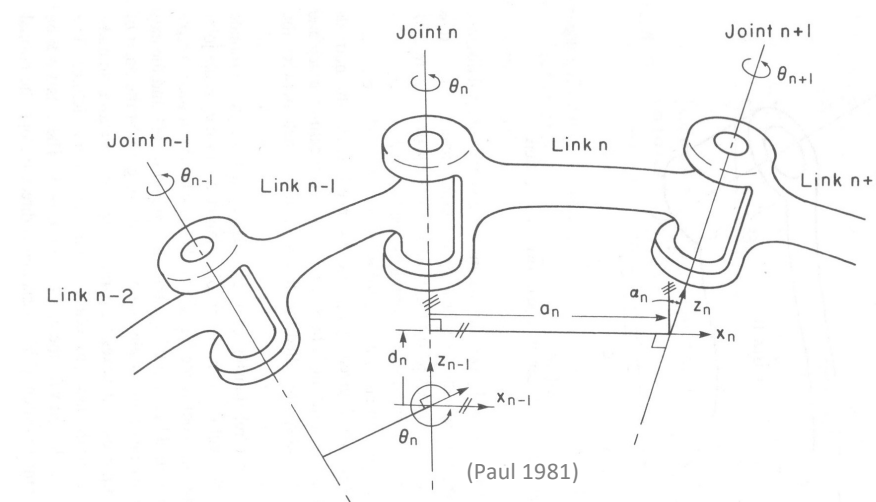
- The **origin** of each coordinate frame of **link n** is set to be at the intersection of the common normal between the axes of **joints n and $n+1$** and the axis of joint **$n+1$**



Denavit-Hartenberg Representation

Assign coordinate frames to each link

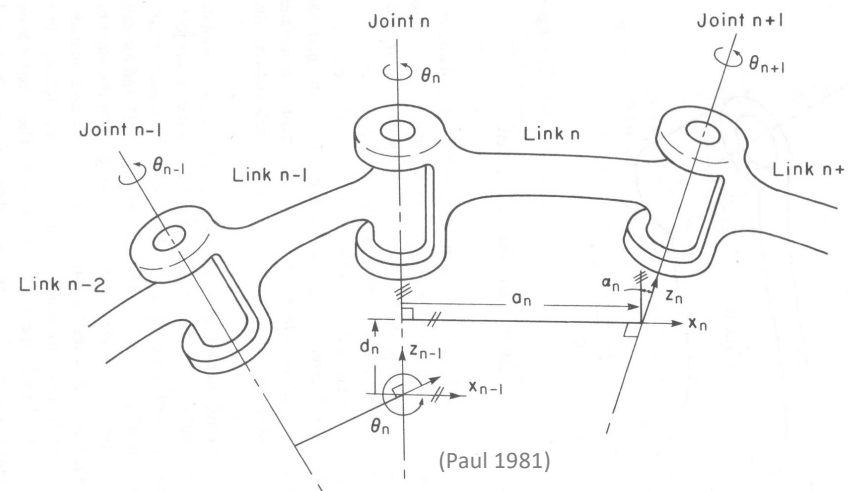
- In the case of **intersecting joint axes**, the origin is at the point of intersection of the joint axes



Denavit-Hartenberg Representation

Assign coordinate frames to each link

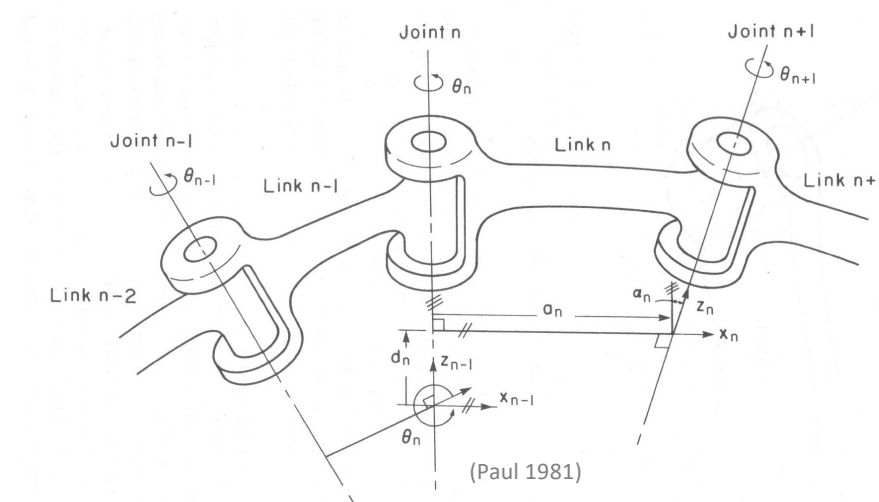
- In the case of **parallel joint axes**, the origin is chosen to make the joint distance zero for the next link whose coordinate origin is defined



Denavit-Hartenberg Representation

Assign coordinate frames to each link

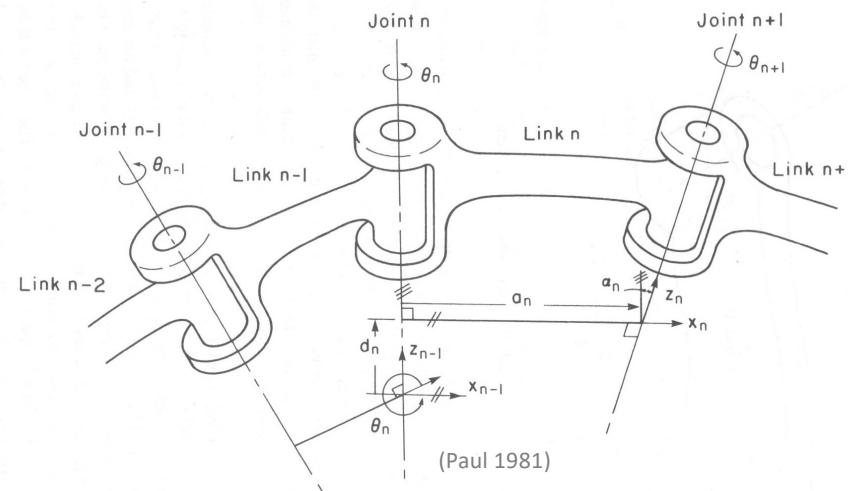
- The Z axis for link n will be aligned with the axis of joint $n+1$



Denavit-Hartenberg Representation

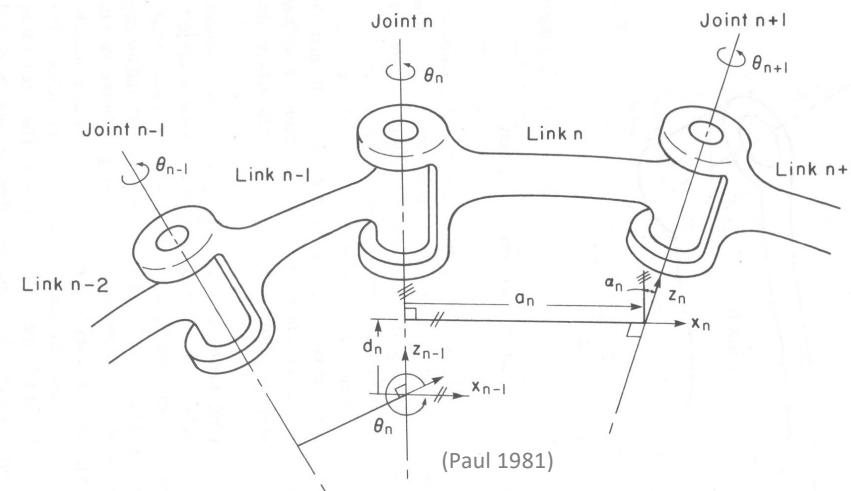
Assign coordinate frames to each link

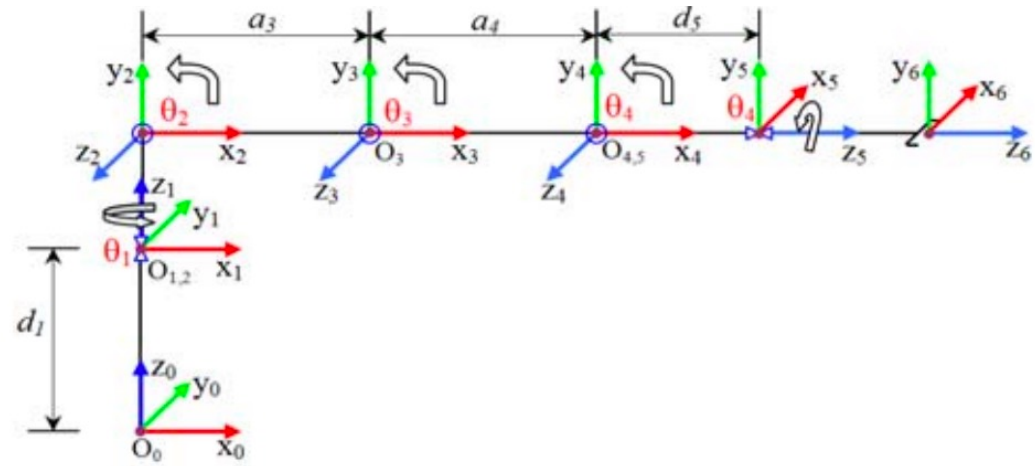
- The X axis will be aligned with any common normal which exists and is directed along the normal from joint n to joint $n+1$



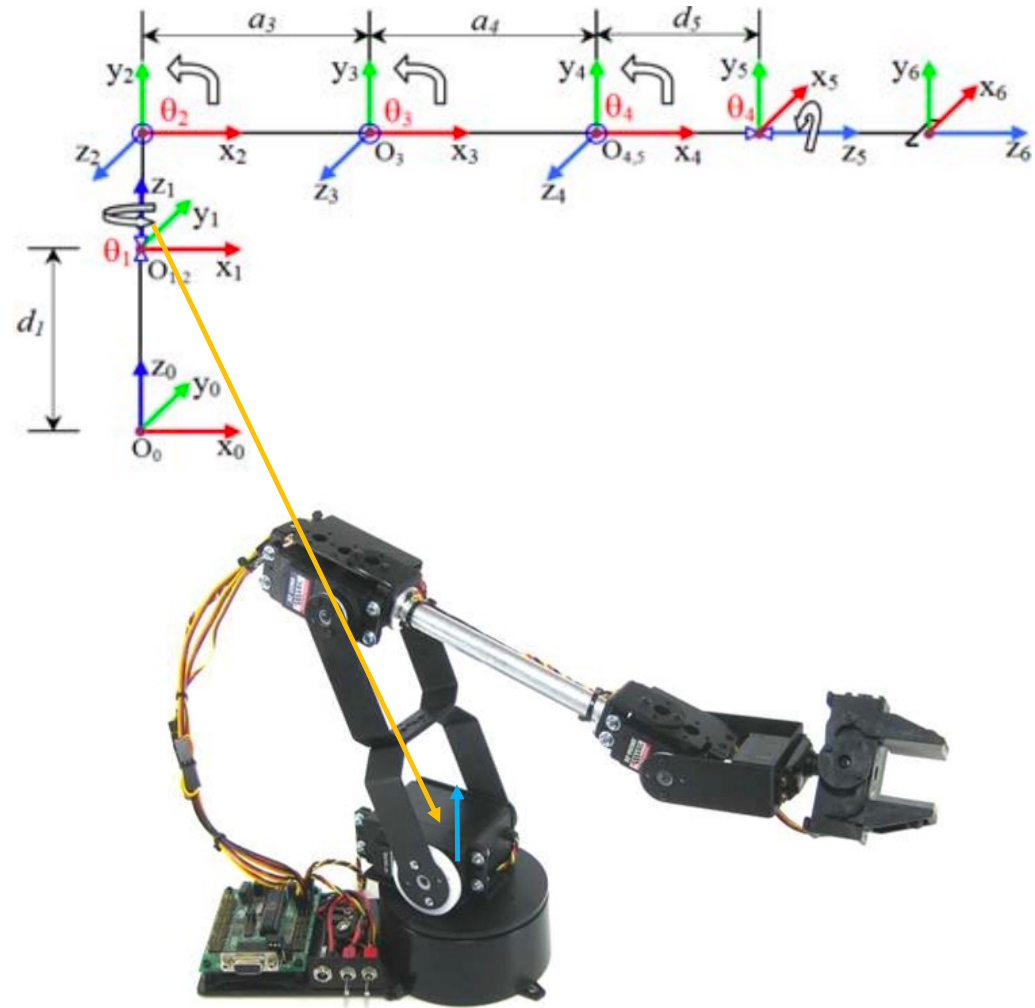
Denavit-Hartenberg Representation

- The base is considered to be link 0
- Link 1 is joined to the base (link 0) by joint 1

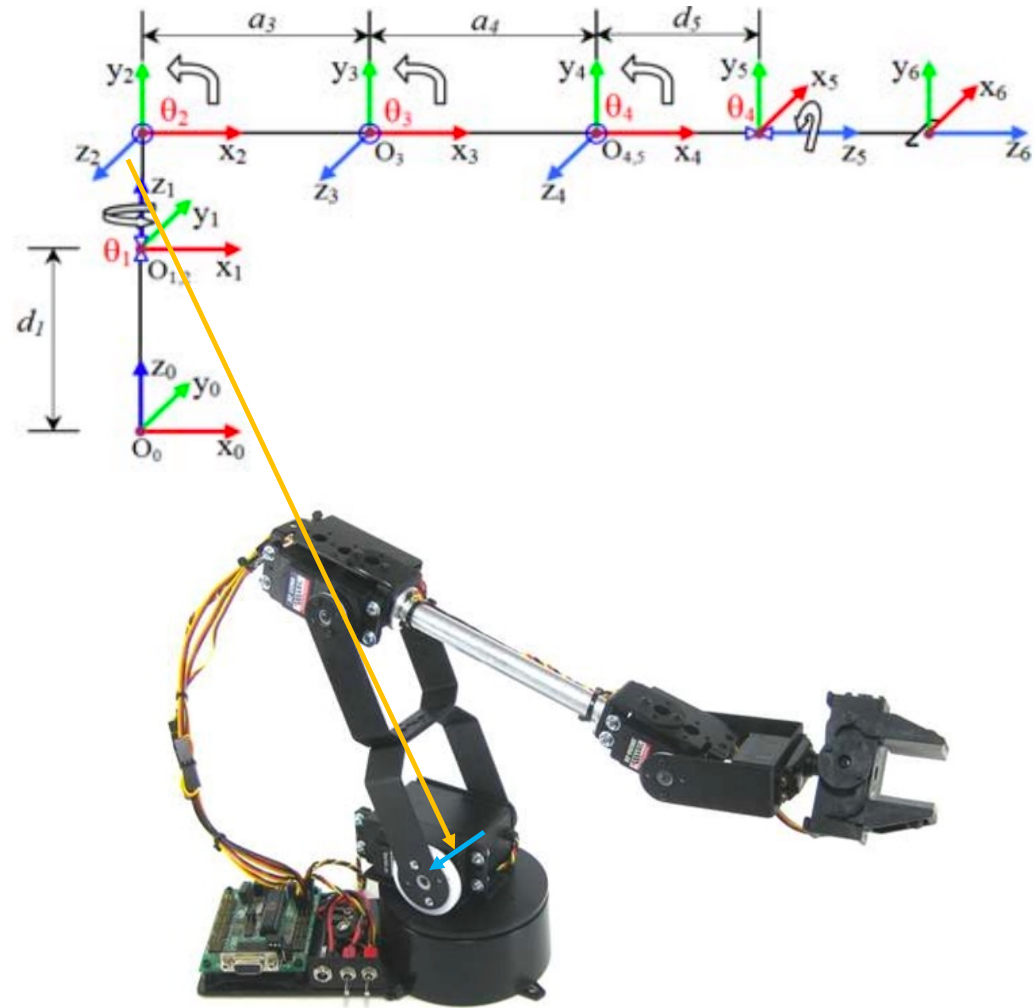




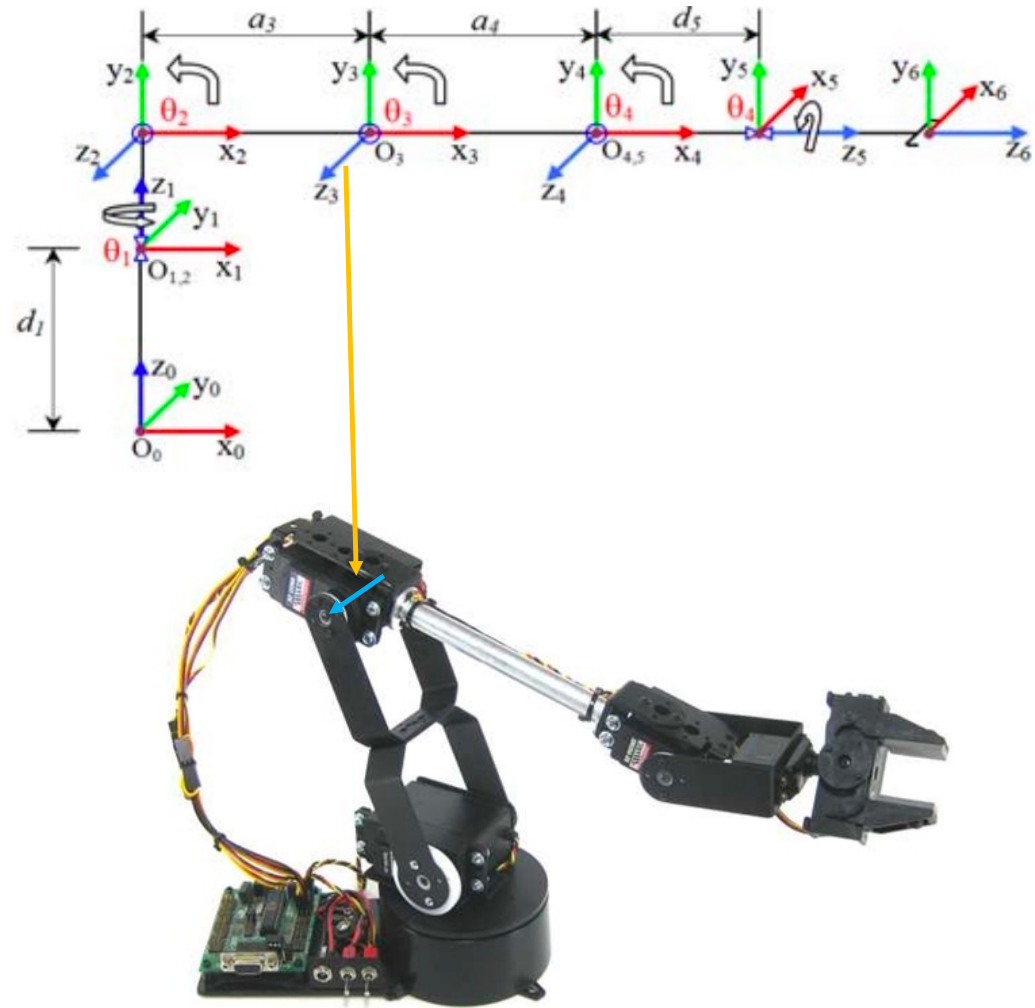
M. A. Gasseem, I. Abuhadrous, and H. Elaydi, "Modeling and Simulation of 5 DOF educational robot arm", 2nd International Conference on Advanced Computer Control (ICACC), 2010.



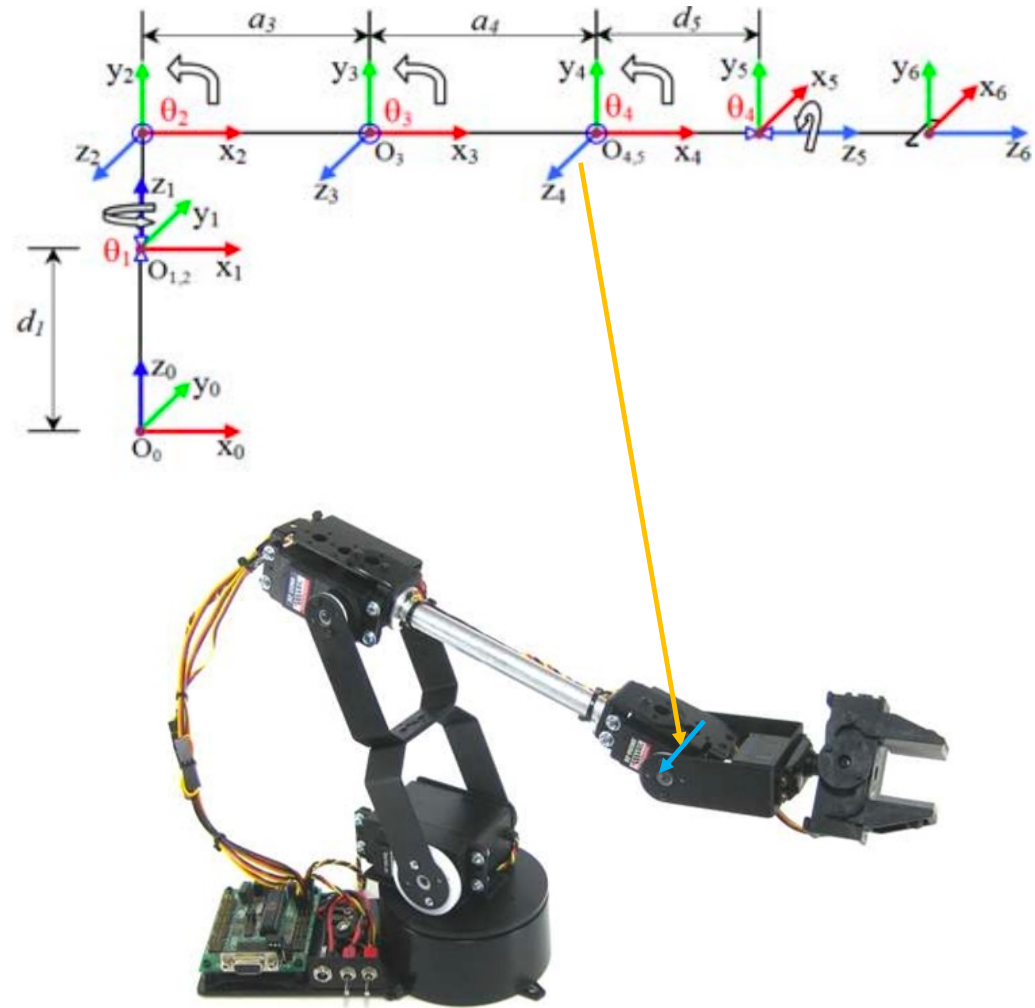
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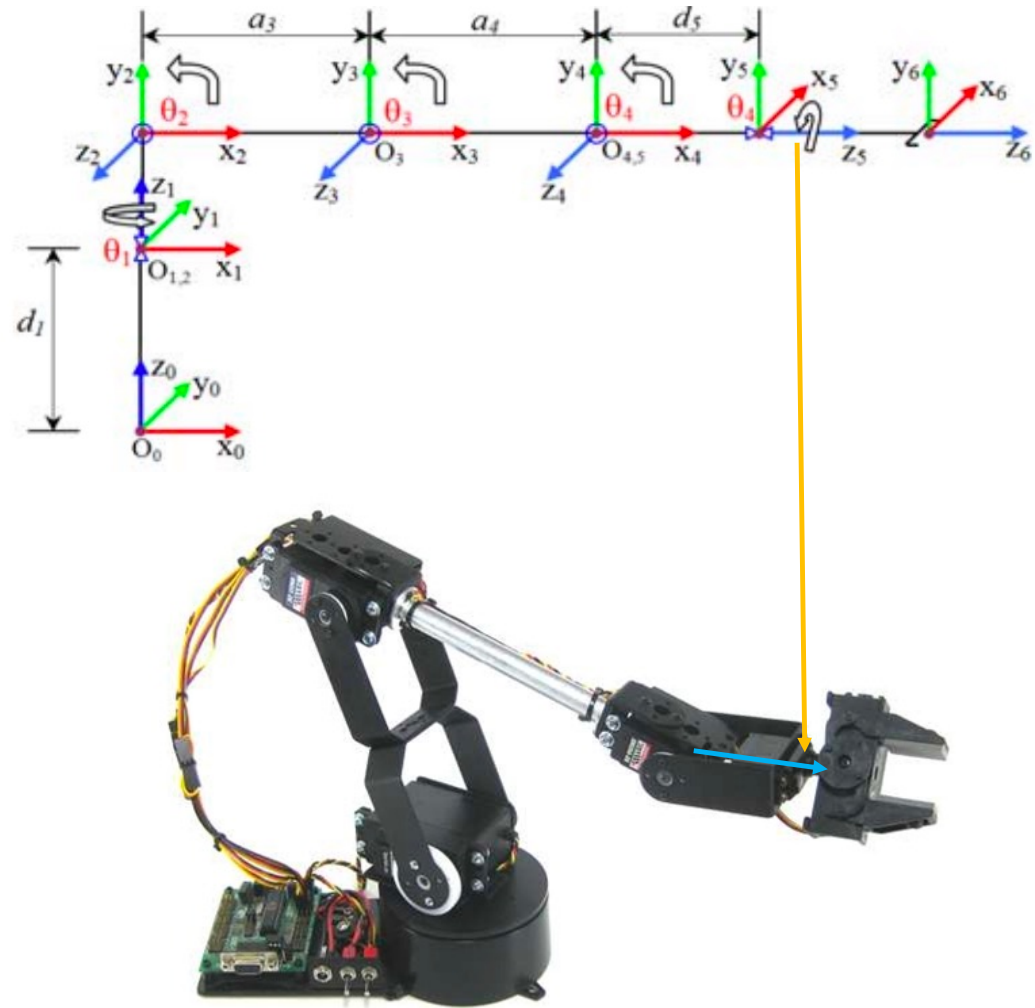
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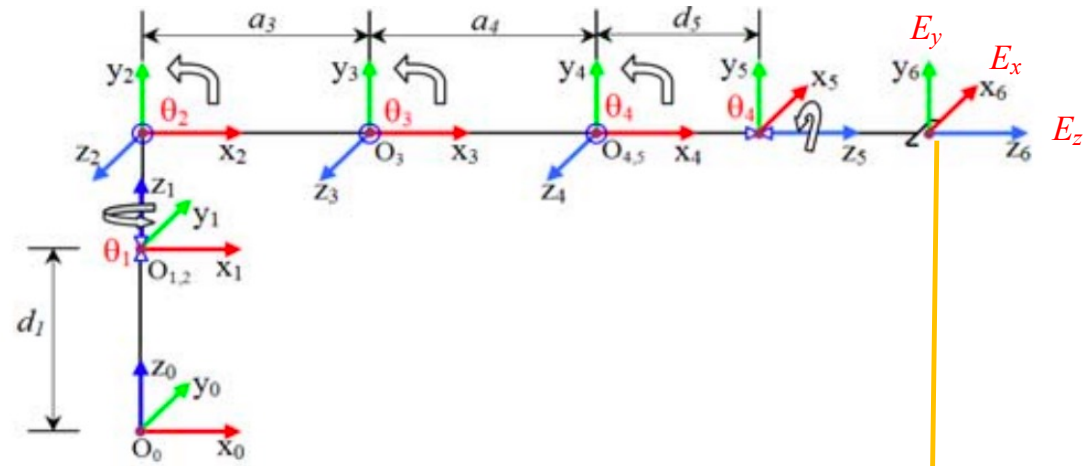
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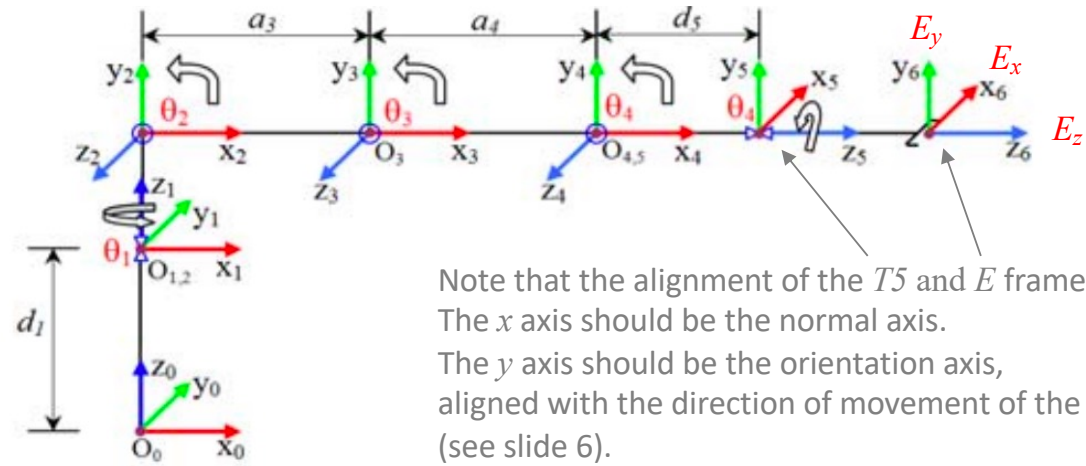
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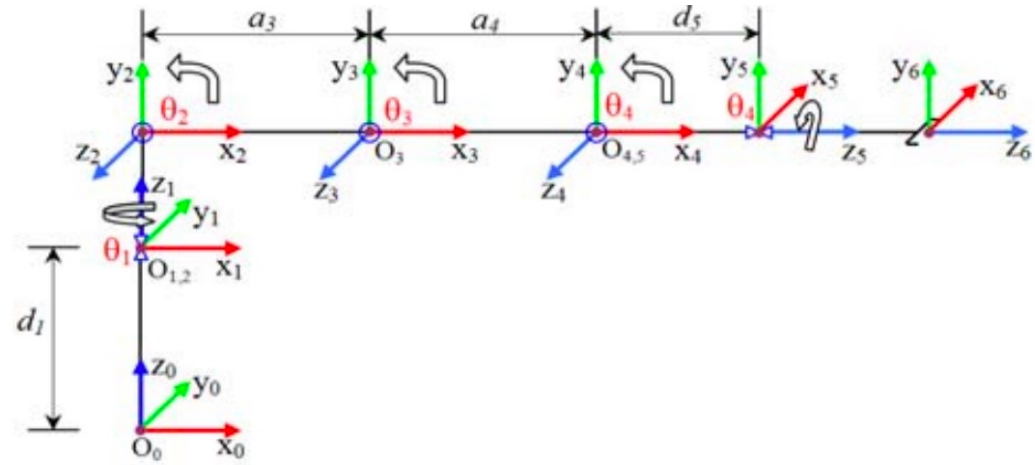
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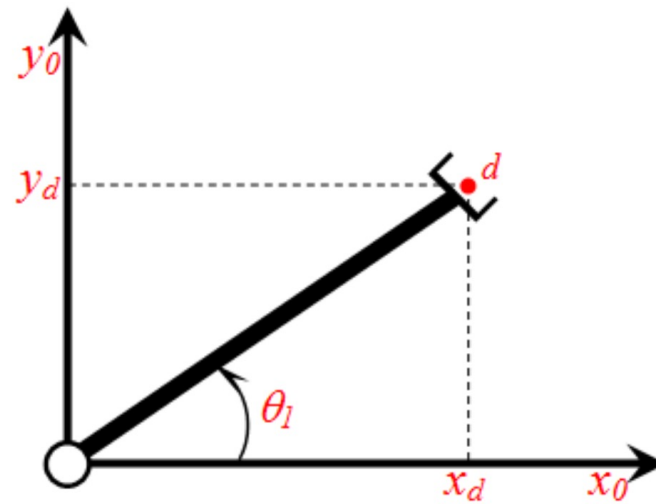


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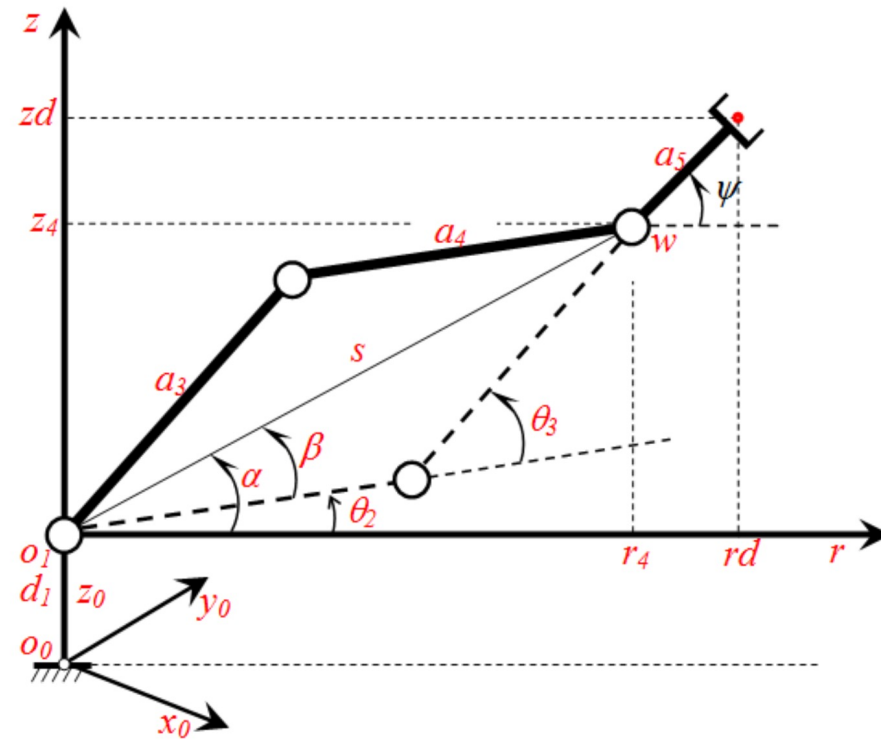
i	α_{i-1}	a_{i-1}	d_i	θ_i
1	0	0	d_1	θ_1^*
2	90	0	0	θ_2^*
3	0	a_3	0	θ_3^*
4	0	a_4	0	$\theta_4 - 90^*$
5	-90	0	d_5	θ_5^*
6	0	0	0	Gripper

M. A. Gassem, I. Abuhadrous, and H. Elaydi, "Modeling and Simulation of 5 DOF educational robot arm", 2nd International Conference on Advanced Computer Control (ICACC), 2010.



$$\theta_1 = \text{Atan2}(y, x)$$

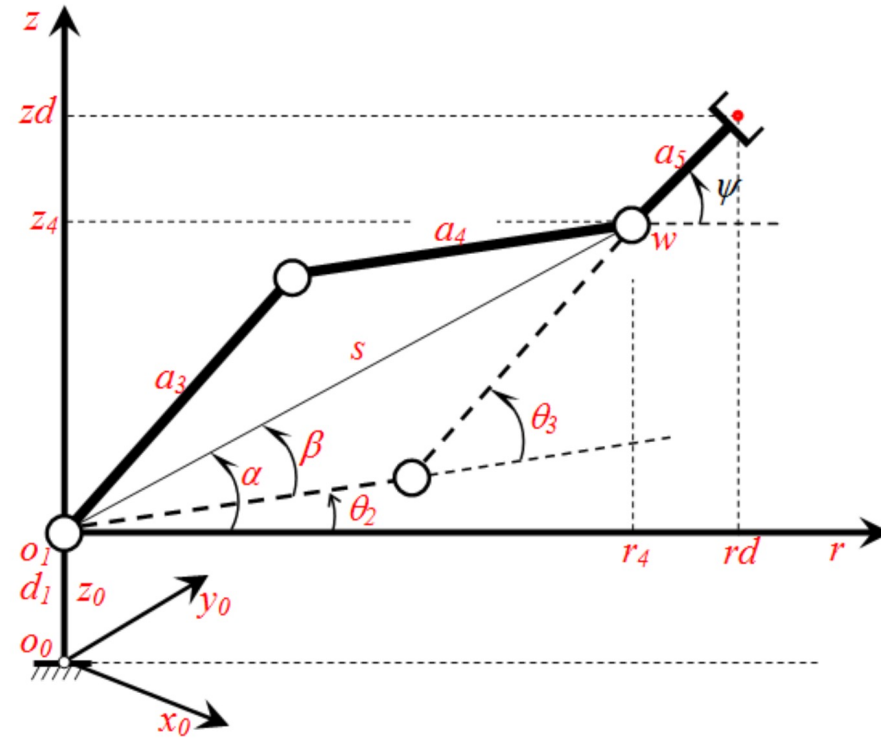
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$$r_4 = a_3 \cos(\theta_2) + a_4 \cos(\theta_2 + \theta_3)$$

$$z_4 = a_3 \sin(\theta_2) + a_4 \sin(\theta_2 + \theta_3) + d_1$$

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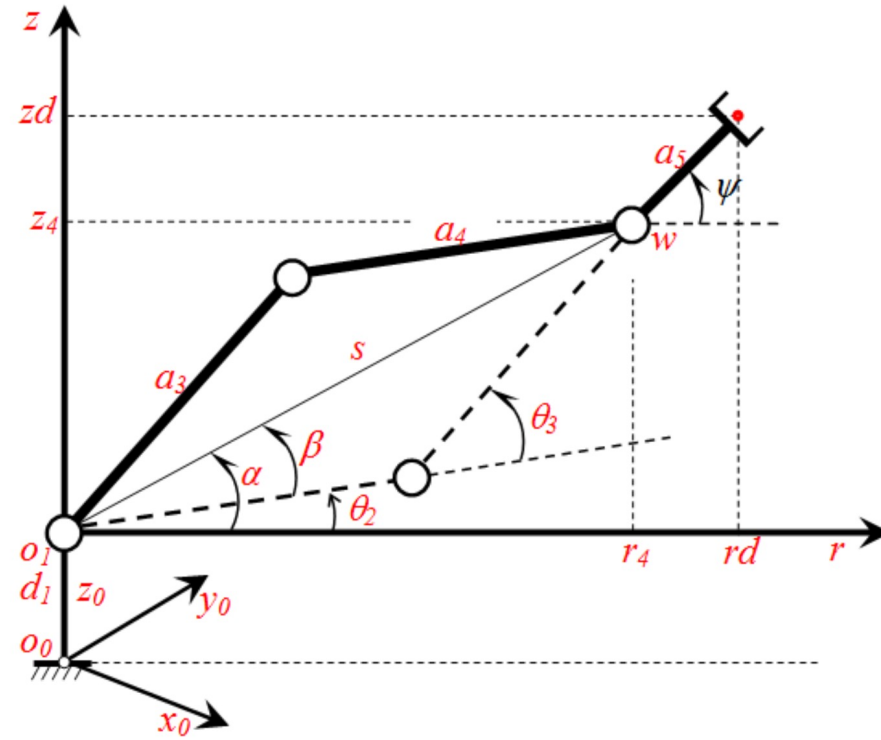


$$\beta = A \tan 2(s^2 + a_3^2 - a_4^2, 2sa_3)$$

$$\alpha = A \tan 2(z_4 - d_1, r_4)$$

$$s = \sqrt{(z_4 - d_1)^2 + r_4^2}$$

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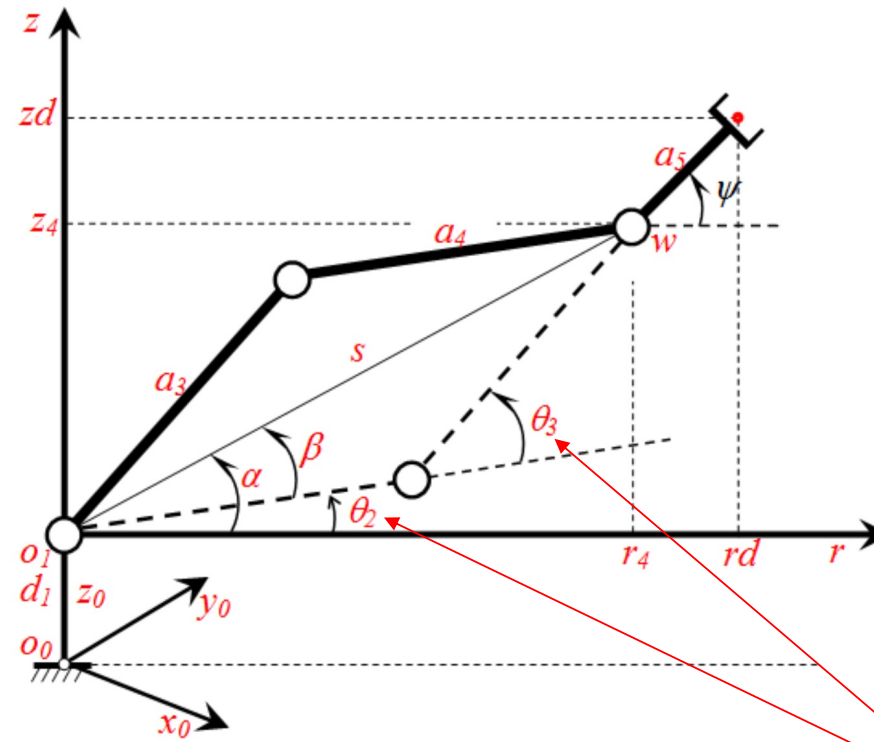


$$\theta_2 = \alpha \pm \beta$$

$$\theta_3 = A \tan 2(s^2 - a_3^2 - a_4^2, 2a_3a_4)$$

$$\theta_4 = \psi - \theta_2 - \theta_3$$

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$$\theta_2 = \alpha \pm \beta$$

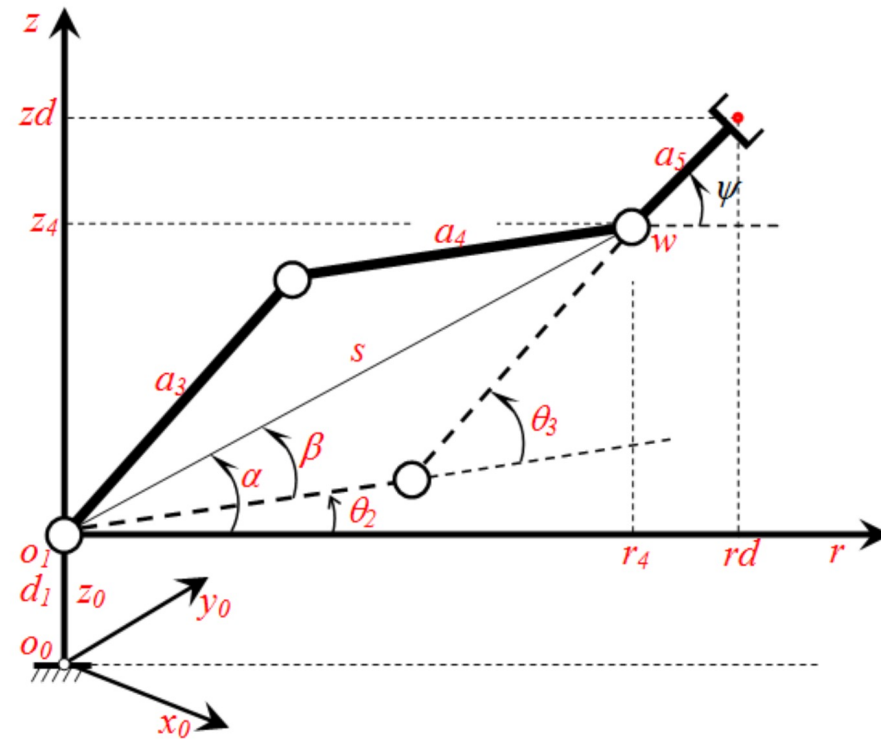
$$\theta_3 = A \tan 2(s^2 - a_3^2 - a_4^2, 2a_3a_4)$$

$$\theta_4 = \psi - \theta_2 - \theta_3$$

This equation for θ_3 is valid for the case where $\theta_2 = \alpha - \beta$. i.e. the case shown in the diagram

It should be negated for the case where $\theta_2 = \alpha + \beta$ i.e. the solution used in the inverse kinematics in the code provided in the accompanying software

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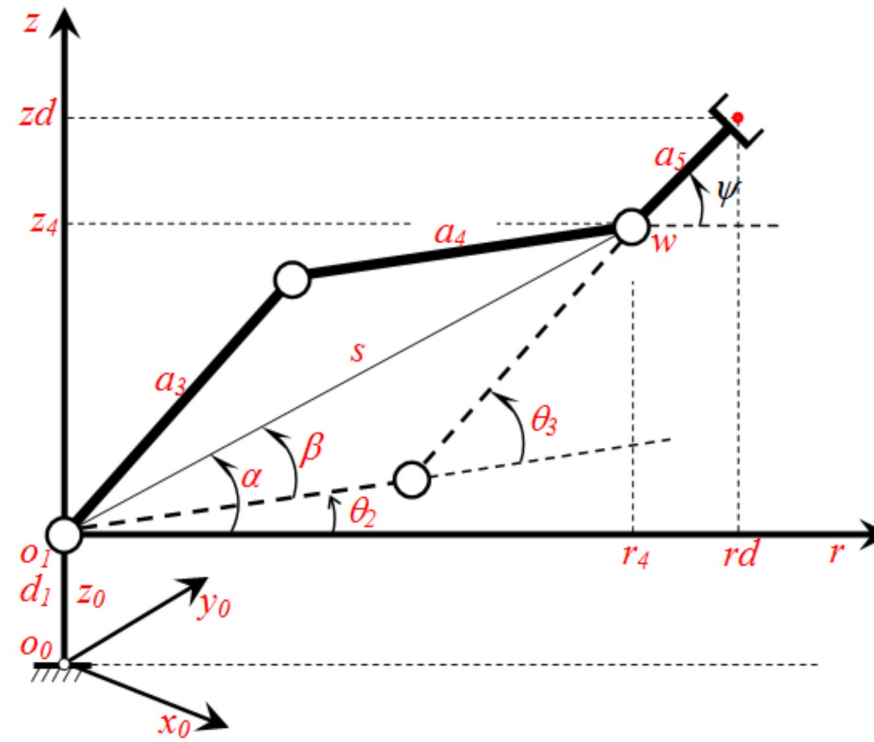
$$\theta_2 = \alpha \pm \beta$$

$$\theta_3 = A \tan 2(s^2 - a_3^2 - a_4^2, 2a_3a_4)$$

$$\theta_4 = \psi - \theta_2 - \theta_3$$

Adjust θ_4 by +90 degrees to if you want to have the T5 z axis aligned with the base frame of reference z axis when T5 is a pure translation

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There is no expression for θ_{\square}
It is assumed that it is given,
and used directly.

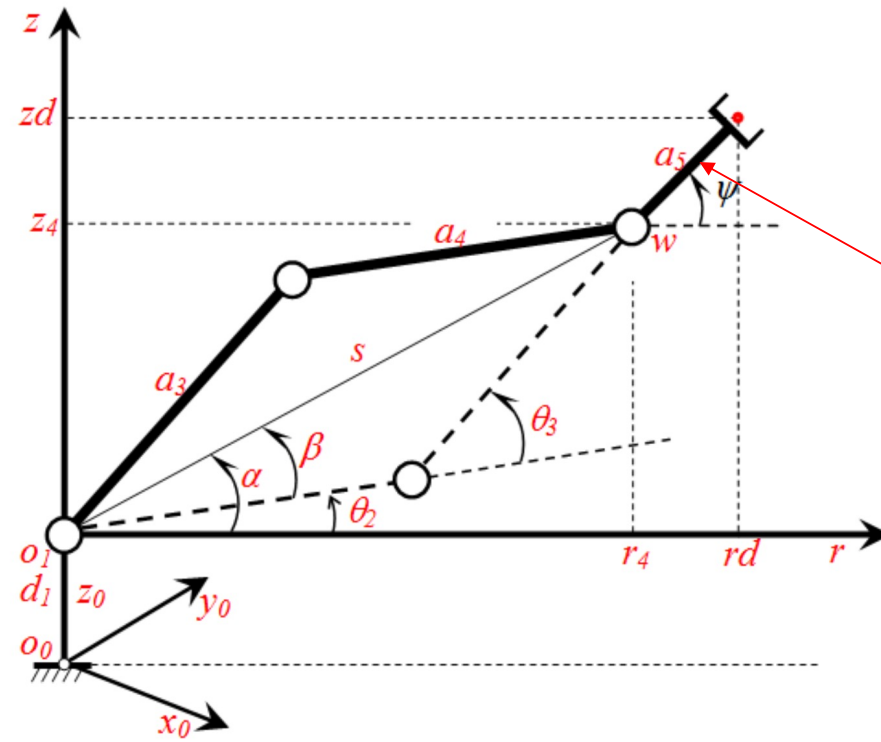
Adjust θ_{\square} by +90 degrees to if you want to have the
T5 z axis aligned with the base frame of reference z
axis when T5 is a pure translation

$$\theta_2 = \alpha \pm \beta$$

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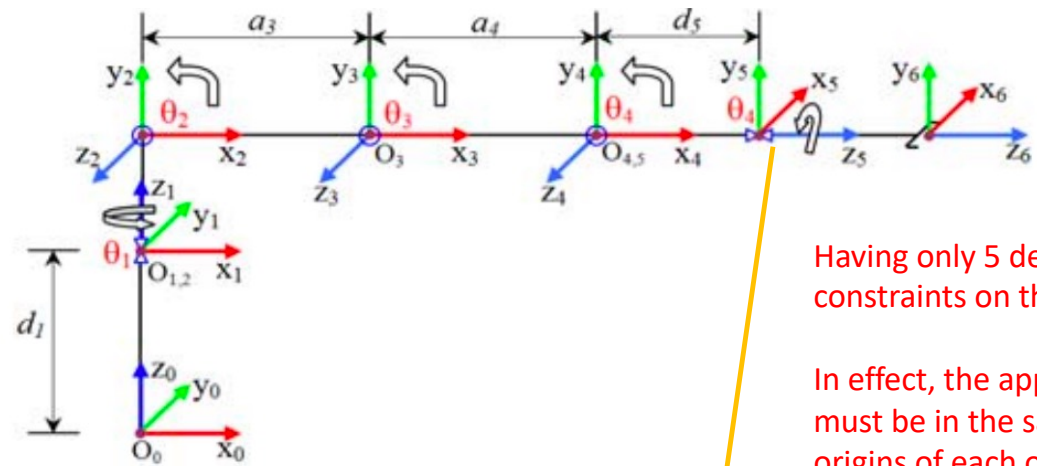
d_5 is not used in this solution (the a_5 is a typo in the figure). It is effectively integrated into the end-effector frame E so that the origin of T_5 is in the wrist, where it should be, and not in the gripper as shown.

$$\theta_2 = \alpha \pm \beta$$

$$\theta_3 = A \tan 2(s^2 - a_3^2 - a_4^2, 2a_3a_4)$$

$$\theta_4 = \psi - \theta_2 - \theta_3$$

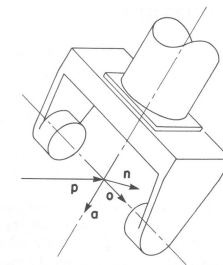
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Having only 5 degrees of freedom imposes constraints on the achievable pose.

In effect, the approach vector a of the T5 frame must be in the same plane as that formed by the origins of each of the manipulator links.

Orienting a vertically upwards or downwards satisfies this requirement.



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